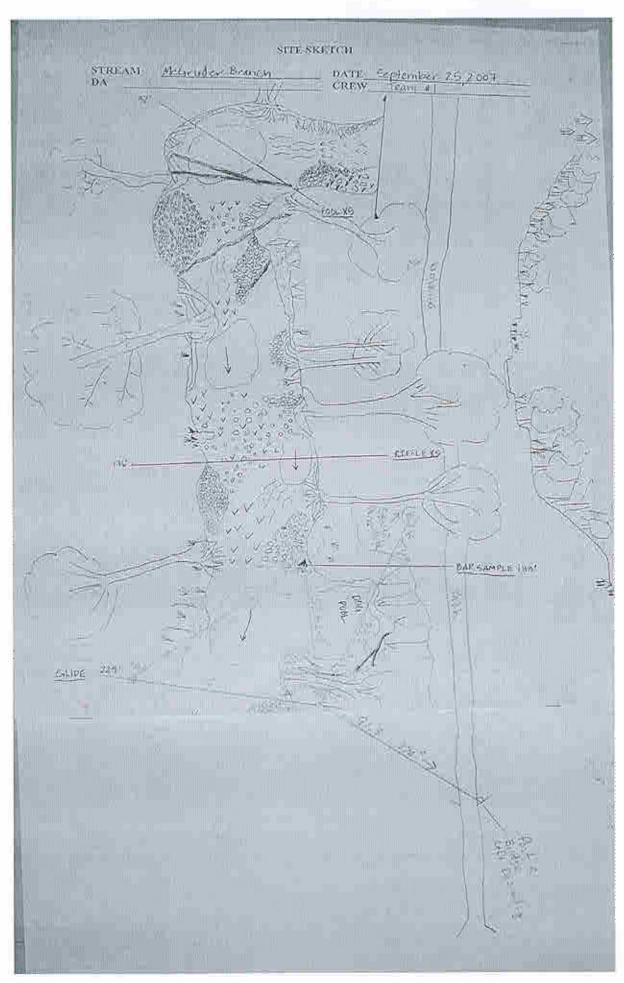
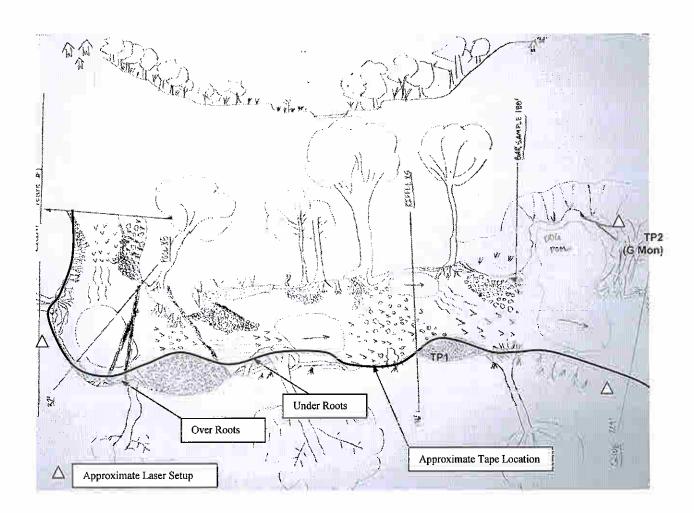
River Assessment and Monitoring NCTC - Shepherdstown, WV 9/17 – 9/27/2007

Team 1
Day 3
Magruder Branch
Degraded Reach

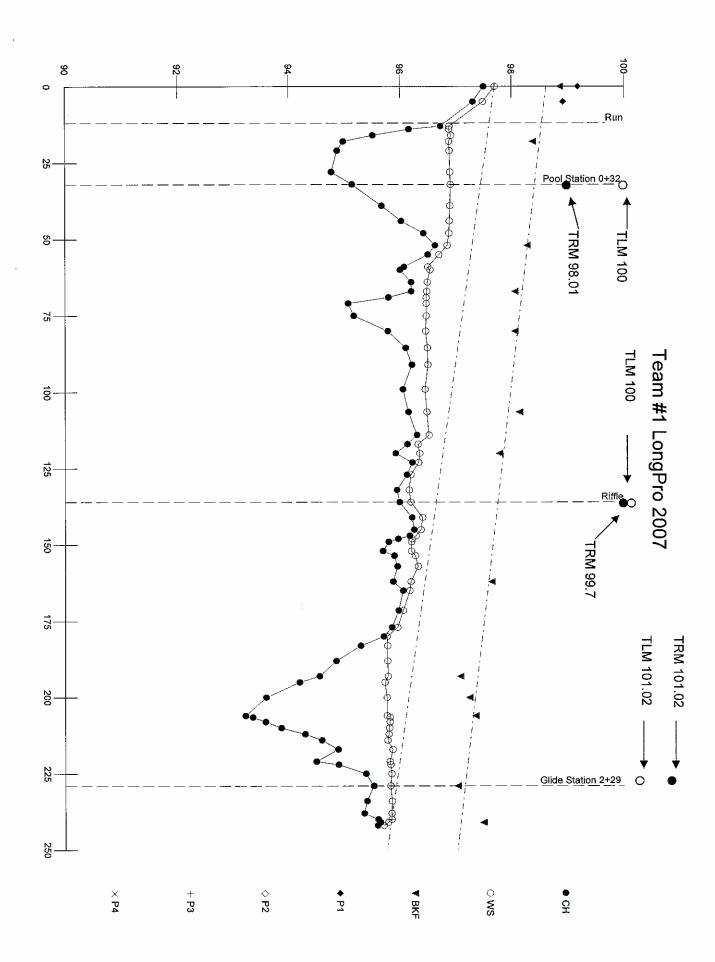


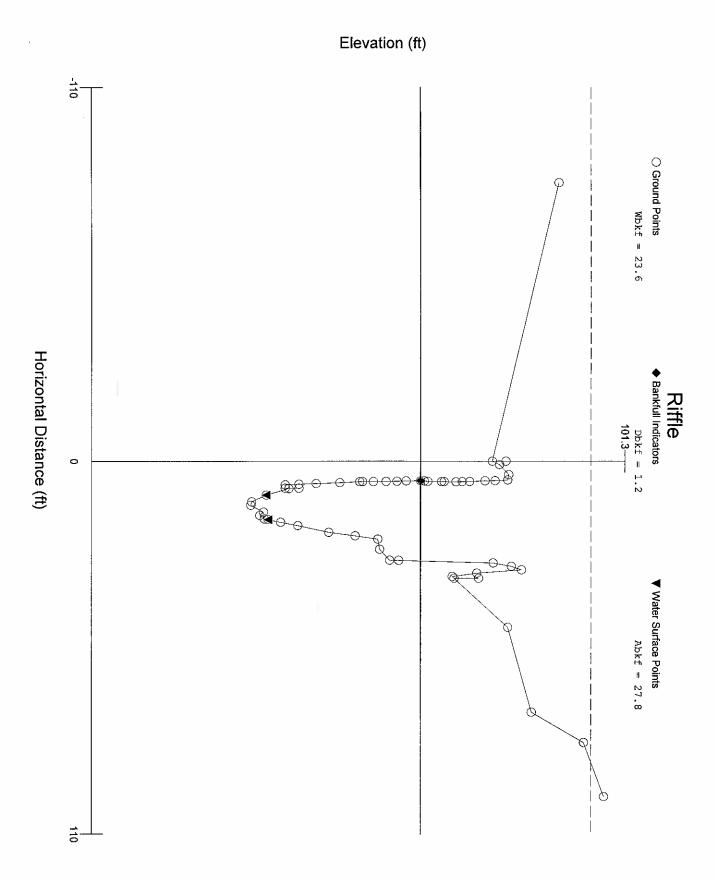
Longitudinal Profile Notes

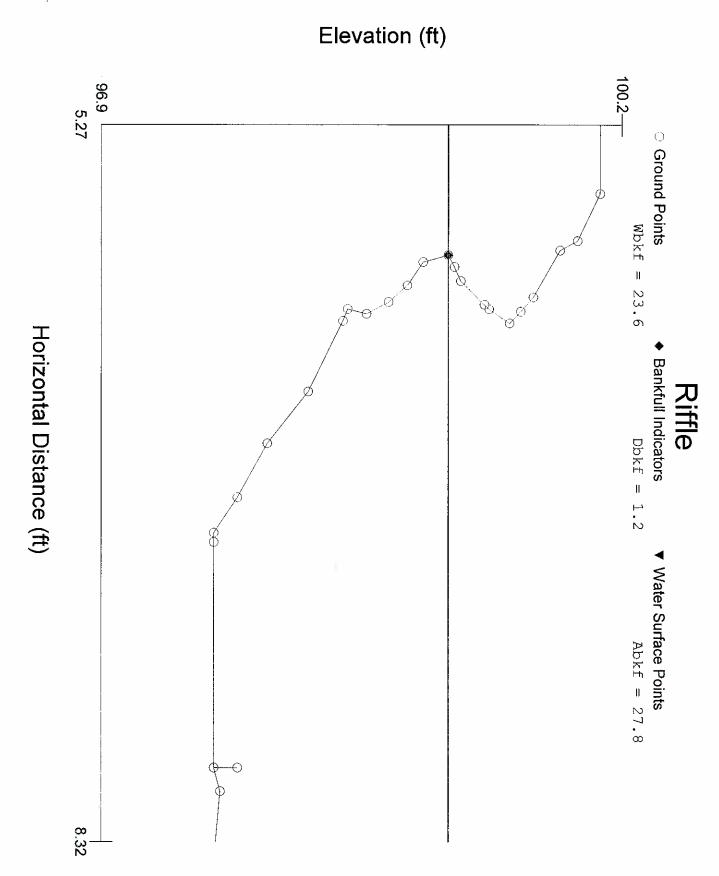
- Tape was placed along the right low flow channel bank.
 - o Tape was placed up and over large tree near approx. station 50
 - o Tape was placed under the exposed roots of the tree upstream of the riffle cross section (shown on geomorphic sketch).
- Utilized three (3) turning points
 - o First turn was made off of an entrained rock downstream of the riffle cross section
 - Second turn was made off of the left monument station of the glide cross section



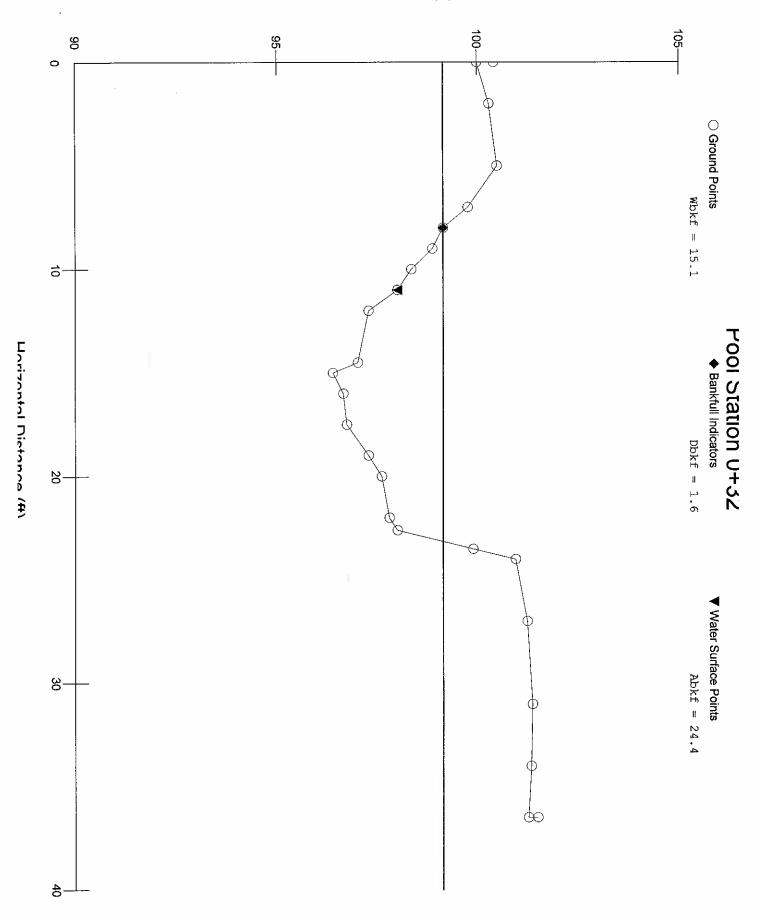
۶,

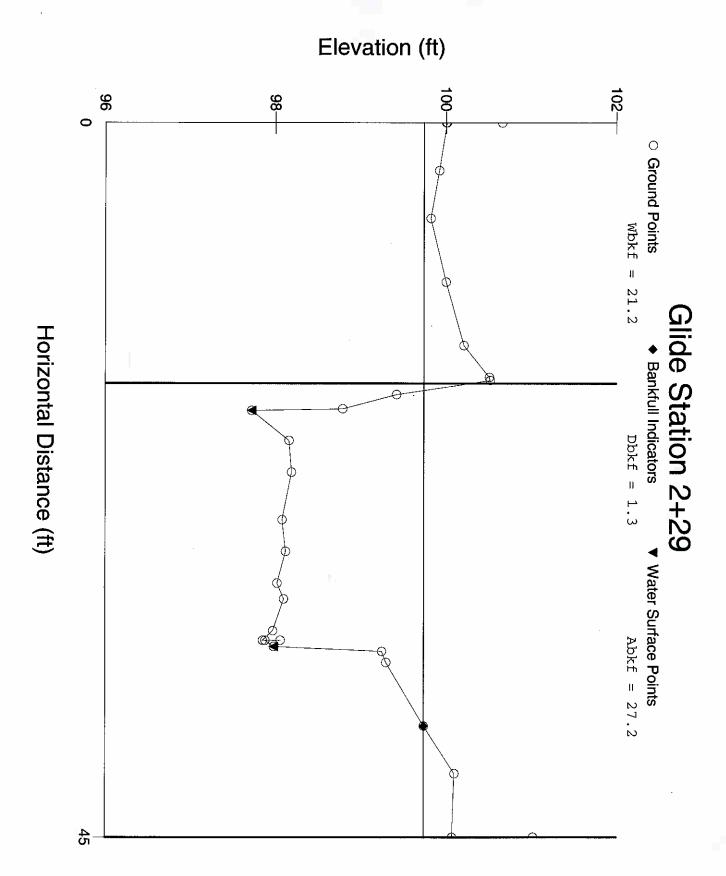




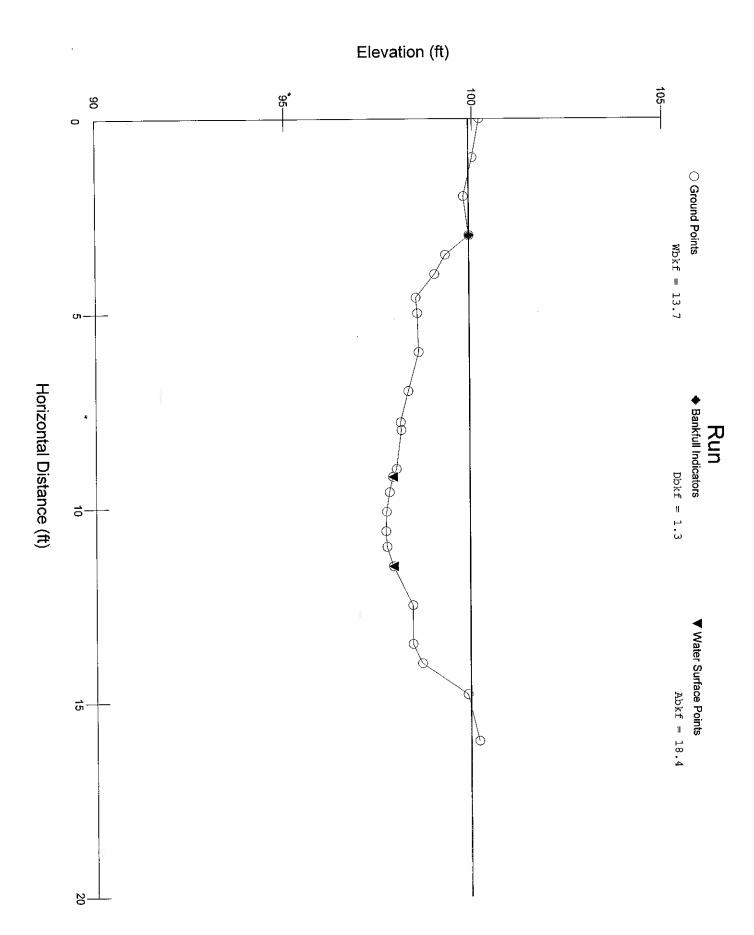


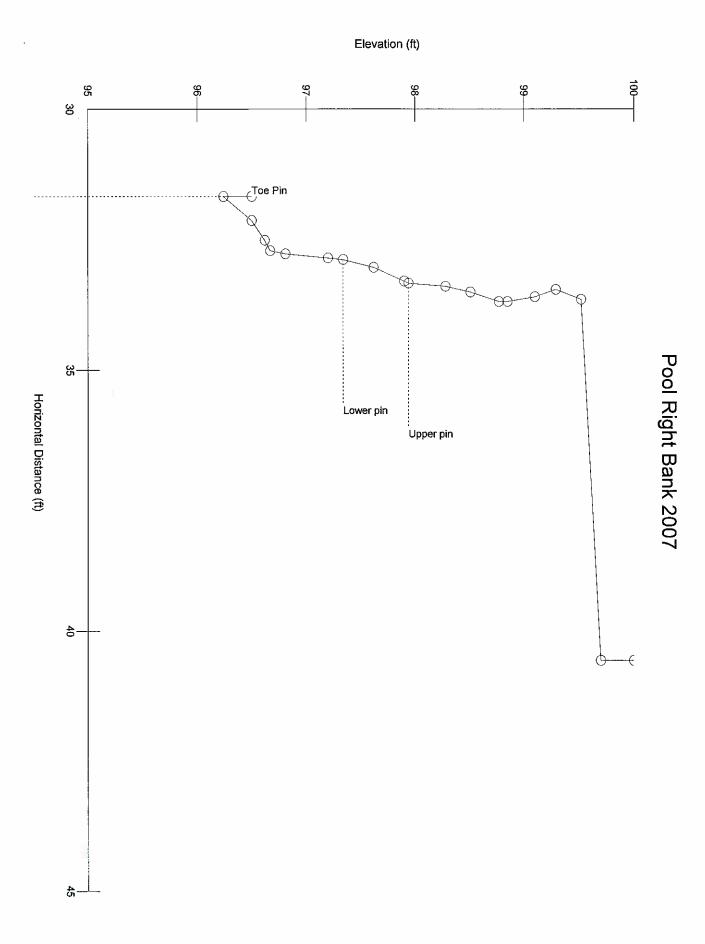
Elevation (ft)



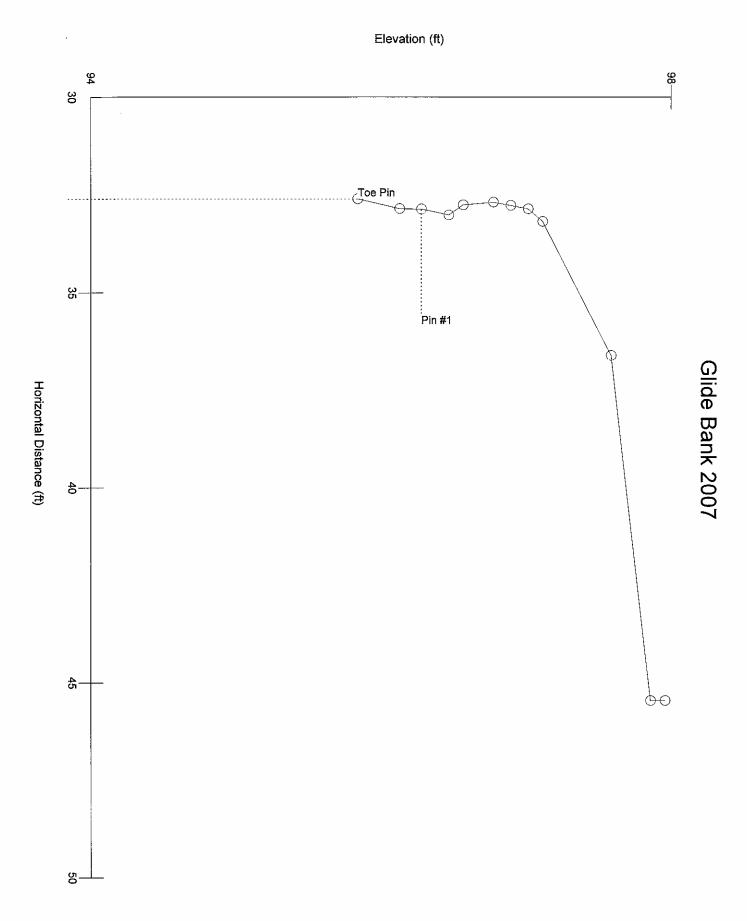


,



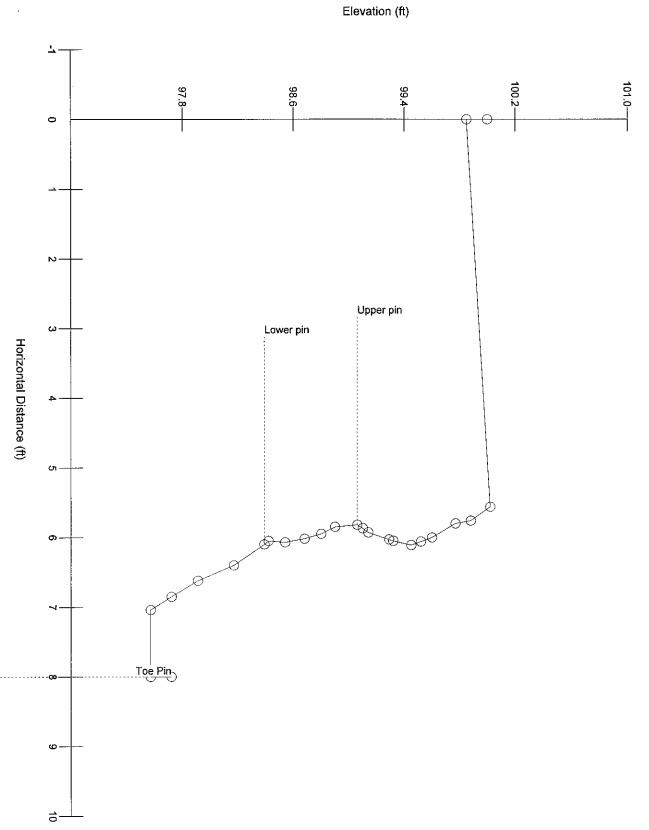


.



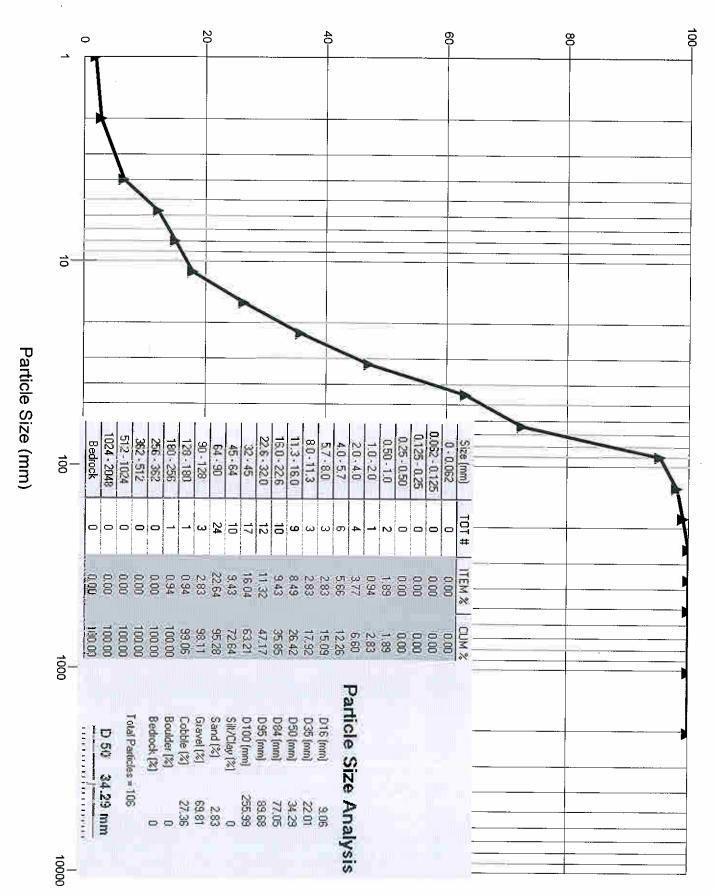
•



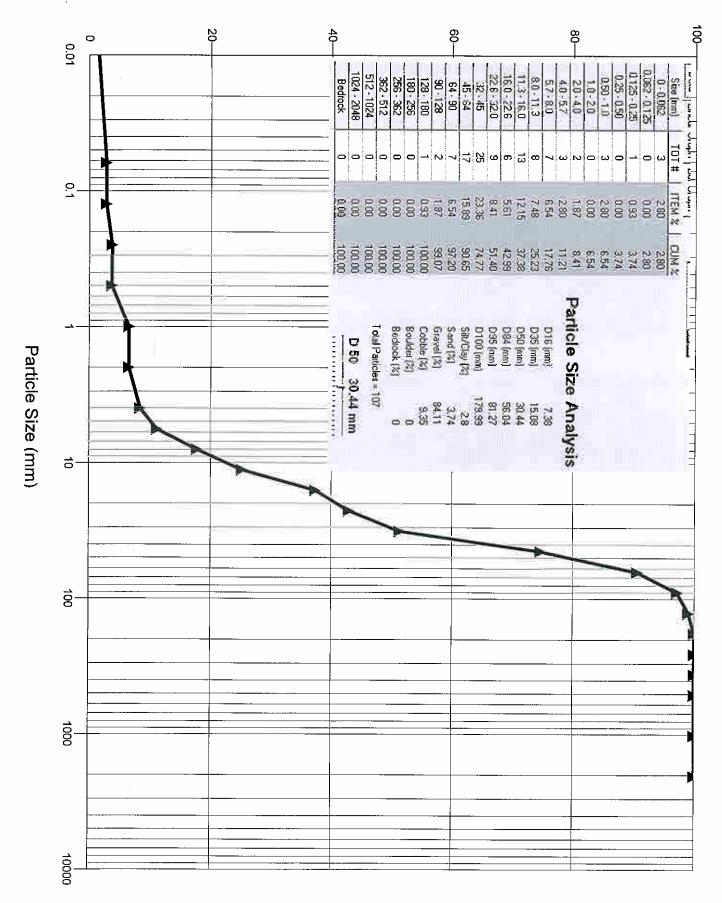


Active Channel

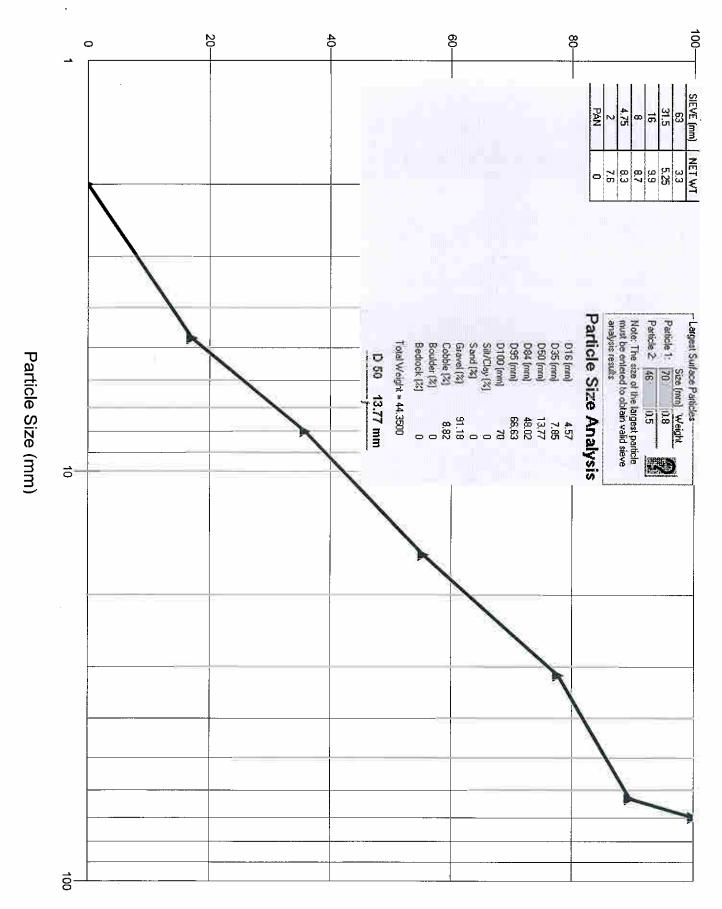
Percent Finer



Percent Finer

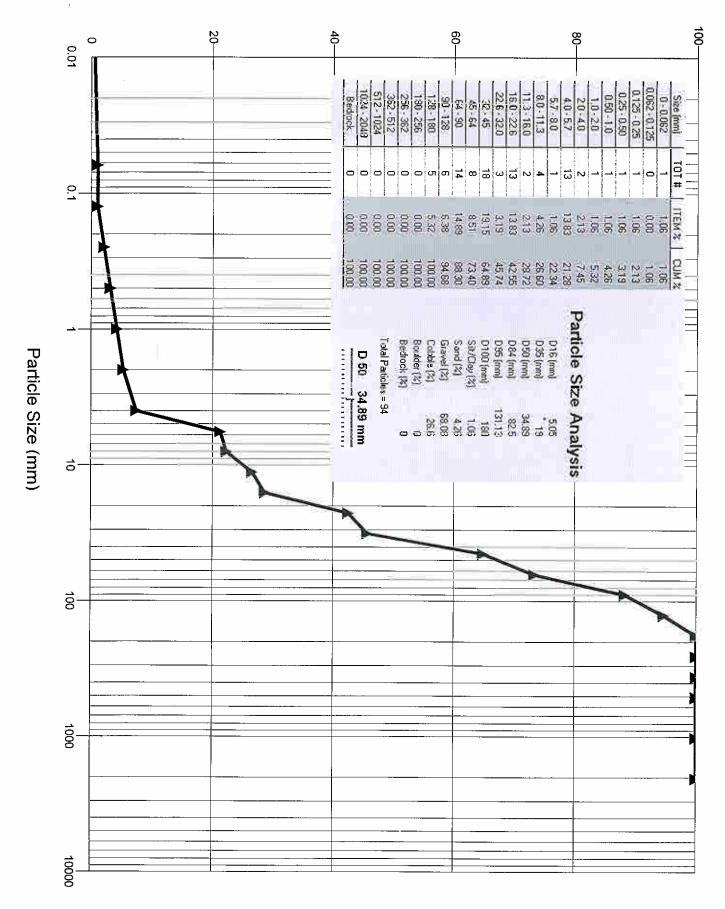


Percent Finer

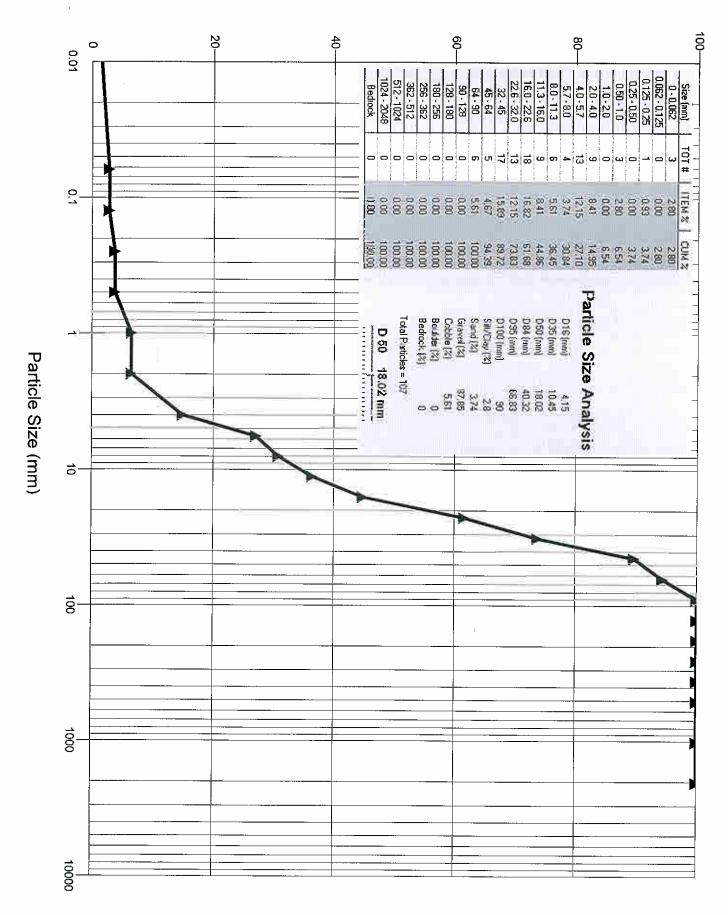


Bar

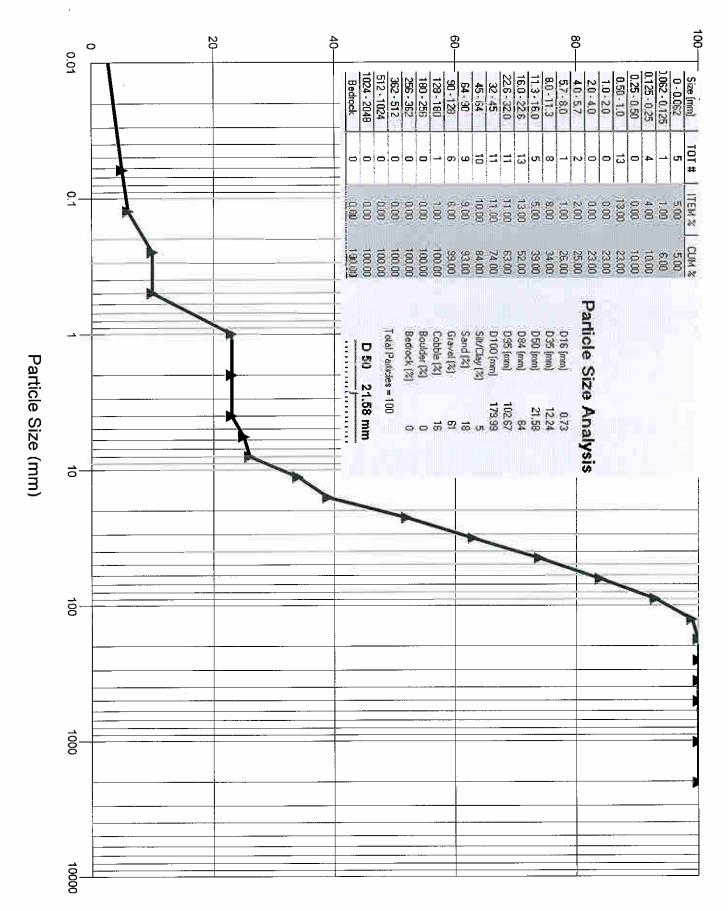
Percent Finer



Percent Finer



Percent Finer



Worksheet 5-3. Field form for Level II stream classification (Rosgen, 1996; Rosgen and Silvey, 2005).

Stream:	Macgruder Day 3, Reach - Reach 1		
Basin:	Drainage Area: 704 acres	1.1	mi ²
Location:			
Twp.&Rge:	; Sec.&Qtr.: ;		
Cross-Sect	ion Monuments (Lat./Long.): 0 Lat / 0 Long	Date	9/26/200
Observers:		Valley Type:	
5	Bankfull WIDTH (W _{bkf})		1
	WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	23.62	ft
	Bankfull DEPTH (d_{bkf}) Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ($d_{bkf} = A / W_{bkf}$).	1.18	ft
	Bankfull X-Section AREA (A _{bkf}) AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	22.22	
	Width/Depth Ratio (W _{bkf} / d _{bkf})	27.77]ft ²
	Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section. Maximum DEPTH (d _{mbkf})	20.02]ft/ft]
	Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thaiweg elevations, in a riffle section.	1.87	ft
5	WIDTH of Flood-Prone Area (W _{fpa}) Twice maximum DEPTH, or $(2 \times d_{mbkl}) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.$	170.82	ft
	Entrenchment Ratio (ER) The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH (W _{fpa} / W _{bkl}) (riffle section).	7.23	ft/ft
	Channel Materials (Particle Size Index) D_{50} The D_{50} particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	21.58	mm
3	Water Surface SLOPE (S) Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	0.00645	ft/ft
8	Channel SINUOSITY (k) Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	1.5	
	Stream Type C 4 (See Figure 2-	-14)	

Worksheet 5-4. Morphological relations, including dimensionless ratios of river reach sites (Rosgen and Silvey, 2005).

Ob	servers:				Date:	9/26/2	007		Valle	y Type:	VIII		Stream	n Type:	C 4	
					Rive	er Rea	ch Sumi	mary D	ata							
	Mean Riffle Depth (dык)	i	1.19	ft	Riffle V	Vidth (V	V _{bkf})	23.	61	ft	Riffle A			28.0	0,1	ft ²
E	Mean Pool Depth (dake)	(E	1,61	R	Pool W	ridth (W	house)	15.	14	ft	Pool Ar	rea (A _b	_{(Tp})	24.4	44	n².
Channel Dimension	Mean Pool Depth/Mear Depth	Riffle	1.35	d _{bkfp} / d _{bkf}	Pool W	/idth/Ri	ffle Width		0.64	W _{bkfp} / W _{bkf}	Pool A	rea / Ri	ffle Area	0.8	7	A _{bkfp} /A _b
	Max Riffle Depth (d _{mbkf})		1.4	ft	Max Po	ool Dep	th (d _{mbkfp})		3.88	ft	Max Ri	ffle De	oth/Mean R	iffle Dept	th	1.18
anne	Max Pool Depth/Mean	Riffle D	epth	3.261							Point B	ar Slop	e e			21
ਹੈ	Streamflow, Estimated	Mean V	/elocity	at Ban	kfull Sta	ige (иы	d)	3.2	25	ft/s	Estima	tion Me	ethod	M	annir	ngs
	Streamflow: Estimated	Dischar	rge at I	Bankfull	Stage ((Q _{bkf})		91.	03	cfs	Draina	ge Area		1.1	1	mi ²
								Dime	nelon	loon Co	om eter	Pation		Mean	Min	Max
-	Geometry Meander Length (Lm)		Mean 106	Min 85	127	ft	Meander			THE RESERVE TO SERVE THE PARTY OF THE PARTY	ometry _{bkf})	Tutto:		-	3.60	5.38
٤	Radius of Curvature (R	c)	25	21		ft	Radius o	f Curva	ture/R	iffle Wid	Ith (Rc∧	N _{bkf})		1.06	0.89	1.65
Pattern	Belt Width (W _{bit})		35	30		ft	Meander	Width	Ratio i	(W _{PH} WF	okt)			1.48	1.27	1.74
nel P	Individual Pool Length		39.5	34.1		ft	Pool Len	gth/Riff	le Wid	th				1.67	1.44	1.90
Chan	Pool to Pool Spacing		58.8	46.5	78.9	-	Pool to F	_	_	_	dth			2.49	1.97	3.34
ပ	Riffle Length		8.67	-	12.2		Riffle Ler		_			_		0.37		0.52
-	g. and congui		0.01													
3	Valley Slope (VS)	0.0	109	ft/ft	Averag	ge Wate	er Surface	Siope	(S)	0.0	0645	ft/ft	Sinuosity			1.34
	Stream Length (SL)	24	13	ft	Valley	Length	(VL)			1	66	rt	Sinuosity	(SL/VL)		1.464
	Low Bank Height (LBH)	start end	1.61 1.68	-		Max Ri Deptl			1.19 1.47			-	ght Ratio (B x Riffle Dep		star end	1.353 1.14
	Facet Slopes	Mean	Min	Max							pe Ratio			Mean	Min	Max
į.	Riffle Slope (S _{rif})			0.049		-	Slope/Ave	_						A INC		7 541
Profil	Run Slope (S _{run})	0.064	0.051	0.075	ft/ft	Run S	lope/Aver	age Wa	iter Su	ırface S	lope (S,	un/S)				11.61
Channel	Pool Slope (S _p)	0.001	0.000	0.002	ft/ft	Pool S	Slope/Ave	rage W	ater Si	urface S	lope (S	_p /S)				0.248
Cha	Glide Slope (S _g)	0.001	0.000	0.001	ft/ft	Glide	Slope/Ave	erage V	/ater S	urface S	Slope (S	S _g /S)		0.078	BARRY III	0.153
	Feature Midpoint *	Mean	Min	Max	1.	lo:m	D				th Rati	09		Mean	Min	Max
	Riffle Depth (d _{rif})	1.4		1.55	_		Depth/Me	PR 160				-		1.18	0.99	
	Run Depth (d _{run})			1.71			epth/Mea					_		1.36		
	Pool Depth (d _p)		3.67			1	Depth/Mea							3.26		_
_	Glide Depth (dg)	1.69	1.52	1.79	[ft	[Glide	Depth/Me	an Riffl	e Dep	tn (d _g /d	l _{bkf})			1.42	1.28	1.504
		Rea	ach	R	ffle ^c		Bar			ach ⁰	Ri	ffle	Bar			Height"
	% Silt/Clay		5		2.8		0	D ₁₆).73	4	.15	4.57	ļ ()	mm
rials	% Sand	1	18	3	.74		0	D ₃₅	1	2.24	10	.45	7.85)	mm
	% Gravel	6	31	8	7.85	9	1.18	D ₅₀	2	1.58	18	3.02	13.77)	mm
Mate	day a sur	9		=	5.61	8	.82	D ₈₄		64	40	0.32	48.02		0	mm
nel Mate	% Cobble	11	16			1		-04			1				_	
Channel Materials	% Cobble % Boulder		0		0		0	D ₉₅	-	2.67	-	5.83	66.63	1 (0	mm

a Min, max, mean depths are the average mid-point values except pools, which are taken at deepest part of pool.

b Composite sample of riffles and pools within the designated reach.

c Active bed of a riffle.

d Height of roughness feature above bed.

,0059

River Assessment and Monitoring: Impaired Reach

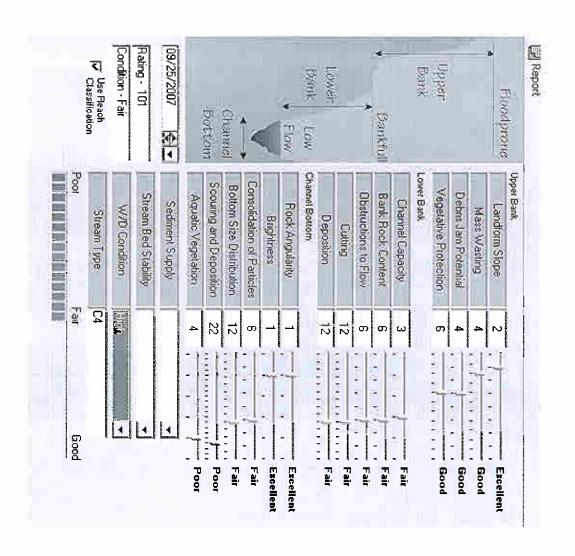
3rd Field Day

Worksheet C-3. Bankfull velocity and discharge estimates:

	Bar	kfull VEL	OCITY /	DISCHA	RGE Estir	nates			Ĭ
Site				Location					ligi 🔻
Date	Stream	Туре	C4	Valley T	уре	VIII			
Observers				HUC	<u> </u>		-		_
INI	PUT VARIA	ABLES			OUTPU	T VARI	ABLES		
Bankfull Cross-s	section AREA	22	A _{bkf} (SqFt)	Bankf	ull Mean Di	ЕРТН	1.0	D _{bkf} . (Ft)	1,5
. Bankfull \		23.3	W _{bkf} (Ft)	Wett	ed PERIME * dbur + Wbur	TER	49.46	W _{Pbkf} (Ft)	70.8
D84 @	Riffle CHAPPING	77.05	Dia. (mm)	D84	4 mm / 304.8	} = '	.2527	D84 (Fi)	
Bankfull	SLOPE	,006	S (Ft / Ft)	Hyd	raulic RADI Abbr/Wpbbr	US.	0.9	R (Ft)	.5
Gravitational A	Acceleration	32.2	g (Ft /Sec ²)		ative Rough R (ft) / D84 (ft)		3.5		1.98
Drainage	AREA	1.0	DA (SqMi)	S	hear Velocit u+ =√gRS	y 	0.42	u* (Ft / Sec)	.312
	ESTIMATION	N METHO	DS		Bankfull V	ELOCITY	Bank DISCH		2.48
1. Friction Rela Factor Roug	tive u = [2. hness	83 + 5.66Lo	g{ R / D84	}]ù*	2.48	Ft / Sec	54,56	CFS	4/4 - 42
2. Roughness Coeffi roughness. u = 1.48			= 6045	·062	2,37	Ft / Sec	35,4 52.15	CFS	M. H
2. Roughness Coeff b) Manning's 'n' fi Note: This equation is for	rom Jarrett (USG	S): n = 0.39S	95* R ^{2/3} *S ^{1/2} ³⁸ R ¹⁶ n boundary roug	- 048		Ft / Sec		CFS	
boulder-dominated stream	n systems; i.e., for stream					in A series			
	rom Stream Type	n = [895* R ²⁵ *S¹ . <mark>ዕ</mark> ዛያ		2.22	Ft / Sec	48.89	CFS	
3. Other Methods, le. l	lydraulic Geometry	(Hey, Darcy-W	eisbach, Chez	y C, etc.)		Ft / Sec		CFS	
3. Other Methods, ie. l	Hydraulic Geometry	(Hey, Darcy-W	eisbach, Chez	y C, etc.)	2,13	Ft / Sec	46,9	CFS	
4. Continuity Equa Return Per	tions: a) Regional Region at the control of the con	onal Curves charge Q =	u = O/A	@35 22	2.54 4.13	Ft / Sec	93.47	CFS	
4. Continuity Equat	ions: b) USG:	S Gage Data	u=Q/A		<i>Y</i>	Ft / Sec		CFS	
Option 1. For sand an avera Option 2. For bould	ge sand dune protru	asure the " pro t sion height (h _{se} nnels: measure	trusion heigh in feet) for t several "pro	at" (h _{sd}) of sar he D84 term i otrusion heigl	nd dunes above in estimation m hts" (h _{bo}) of bo	channel bed ethod 1. ulders above	elevations. Sul channel bed	ostitute	
Option 3. For bedro surfaces a		nnels: measure	several "pro	trusion heigh	nts" (h _{bx}) of roo	k separations	/steps/joints/ u		

6.20

35.8 23.4



16.7

WARSSS page 5-108

Date 09/18/07 (Eug) 0.00 0.03 0.01 0.07 0.01 peoued ans sand transport (tons) 000 6.02 0.03 800 0.01 a edjusted bedloed transport [[13]×[14] t (Eucz) 0.05 0.0 0.0 0.00 8 0.01 0.02 0,03 0.02 0.00 8 000 Gage Station #: 01591000 (presida) 1.68 1% 1.83 7.80 5.60 Total annual sediment yield (bedoad and s is pended sand bed-material load) (tons/yt): 0.00 8.0 0.00 0.10 0.20 0.30 0.00 0.08 0.80 3. 2.30 9.0 (days) (busklay) Time Dally increment mean besided 0.00 040 0.90 8 4.80 0.00 0.00 0.0 0.00 0.00 0.00 0.00 1.70 3,00 Calculate 18.25 36.50 36.50 36.50 36.50 36.50 36,50 36.50 36.50 36,50 3.65 **3** (43) 3,65 3.65 30 *6% 8 20% Š 10% 10% 10% 10% Ē , E <u>*</u> ž 3 è Valley Type: VIII 表が対象 90.0 4 0.13 0.16 0,19 0.34 0,45 0.75 **\$**28 6.22 9.6 0.84 1.02 0.27 26.75 10.08 12,47 17.48 23.67 前庭 2.10 14,21 1.28 88 器が 4.20 5.37 7.23 45.0 2.69 Location Reach 3 (fort) 0.42 0.18 0.26 0,29 0.38 0.06 0.09 0.10 0.1 0.13 0.14 0.16 0.24 0.31 4.4 3 Steam Type: 0.006 0.006 0.006 0.006 000 0.006 0.006 0.006 0.006 0.006 0.006 0.005 0.006 0.006 0.01 (8) 3.26 Ŕ 0.93 1.27 1.69 1.86 2.08 2.35 2.54 2.66 3.07 ** 1.47 Ţ. 2,87 8 Magruder Branch Reference Reach, Reach 3, ref m Hydraufic geometry 0.25 0.30 0.42 0.49 0.58 0.70 0.78 0.95 *** 1.37 ... 0.17 0.27 0.84 6.34 0.38 15.95 11.73 15.84 16.09 16.45 16.72 17.19 12.77 13.44 14.28 15.16 5.66 16.90 16.99 8 æ 6 Wich 21,89 11.44 13.10 14.25 16.27 18.82 2.88 3,5 5.72 £ 1 4.07 8 (#) Catoulate 71.44 14,33 68.30 26.93 33.34 37.96 46.68 57.89 43 3.43 7,18 \$ 1.24 (00) 5.60 4,5 9.04 (2) Deily mean 35,46 12.47 22.45 34,45 40.76 52.60 63.47 Flow duration curve 0.07 2.80 4.0.6 4.97 6.23 8.42 9.35 (90) Team 3 (1) Percentage of 80.0% 70.0% 60.0% 50.0% 40.0% 30.0% 10.0% 40% 10% Observers 5.0% 3.0% 2.0% 1.5% 2

Worksheet 5-12a. Bedload and suspended sand bed-material load transport prediction for the upstream reach, using the POWERSED model

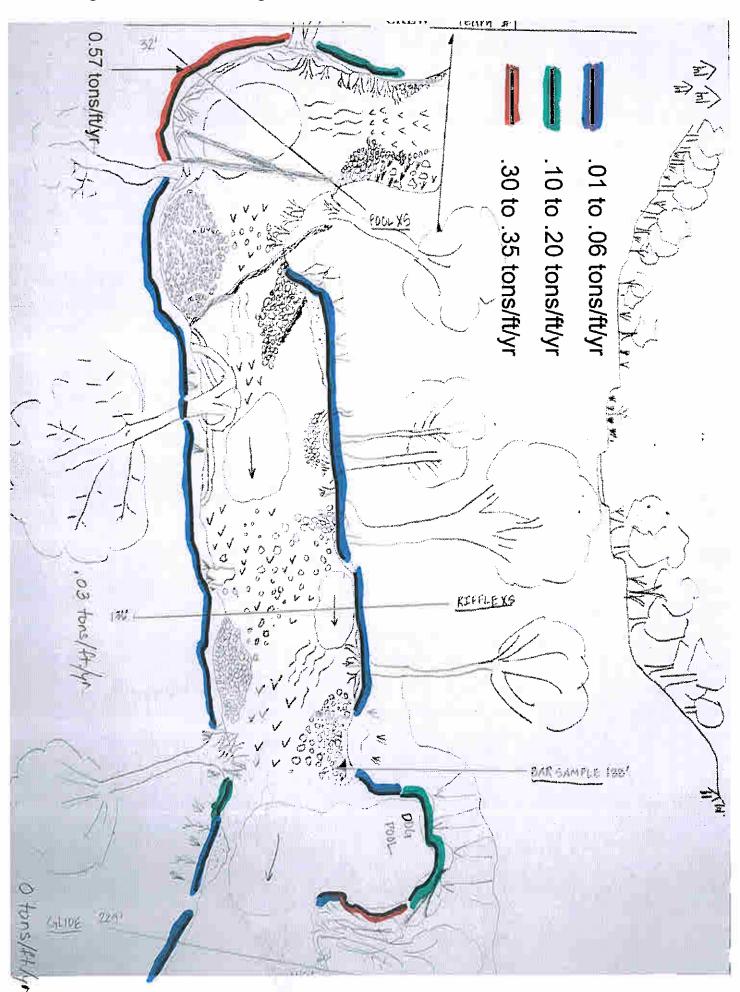
Copyright @ 2006 Wildland Hydrology

WARSSS page 5-109

Worksheet 5-12b. Bedload and suspended sand bed-material load transport prediction for the potentially impaired reach, using the POWERSED model.

Characteries Topin A	Stream	Day 3 - Impaired Reach, Reach 1, Riffle 1+36, (R.	ired Reach	Reach 1	, Riffle 1+	36, Riffe		Location	Location: Reach 3								Pa Tri	09/18/07
The part of the	Observers:	Team3	700 70 00 000	525.575			ŝ	- 1	3	\$	alley Type	5	8	Station #	01581000			
17. 17.	Flow-dur.	ation curve	Calculate		Hydraufic	geometry		Measure					3	loulate				
Columbia Columbia	(1)	(2)	(3)	44	(5)	(9)	(2)	8	(6)	(10)	(11)	(12)	(13)	(14)	(15)	(91.)	(17)	(48)
9. (6.8) (6.8) (6.9) (6.9) (7.9) (7.9) (8.9) (6.9) (7.9) (7.9) (8.9) (6.9) (7.9)	Percentage of time		Mis- ordinate stream- flow		***	Dept	Velocity		394s	awo.	15 d				Delly mean suspended send fars port	adjusted bedbad besport transport ((13) #14))		Tone edjusted total transport [[16]+[17]]
0.0% 0.0 <th>20</th> <th>(\$0)</th> <th>(\$p)</th> <th>(F)</th> <th>•</th> <th>9</th> <th>(SA)</th> <th>(ta)</th> <th>(fr,tj)</th> <th>(\$PQ)</th> <th>(EV.EE)</th> <th>8</th> <th>(\$(ap)</th> <th>(foreign)</th> <th>(/ep/suci)</th> <th>(ters)</th> <th>(Suca)</th> <th>(sug)</th>	20	(\$0)	(\$p)	(F)	•	9	(SA)	(ta)	(fr,tj)	(\$PQ)	(EV.EE)	8	(\$(ap)	(foreign)	(/ep/suci)	(ters)	(Suca)	(sug)
0.00 0.00 <th< td=""><td>100.0%</td><td>20'0</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>86</td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	100.0%	20'0										86						
0% 4.48 3.44 2.87 14.72 0.00 0.00 0.14 14% 38.50 0.00	\$0.0%	2,78	1.42	1,37	8.35	0.16	86.0	90000	90.0	0.53	90'0	40%	36,50	00.0	0.00	0.00	0.00	0.00
0% 4.94 4.49 3.17 11.56 0.27 4.39 0.006 0.14 2.06 0.16 1.06 0.16 0.06 0.07 3.65 0.00 <th< td=""><td>80.0%</td><td>4.03</td><td>3.41</td><td>2.67</td><td>11.21</td><td>0.24</td><td>17</td><td>900.0</td><td>0.09</td><td>1.28</td><td>0.11</td><td>40%</td><td>36.50</td><td>0000</td><td>0.00</td><td>0.00</td><td>0.00</td><td>000</td></th<>	80.0%	4.03	3.41	2.67	11.21	0.24	17	900.0	0.09	1.28	0.11	40%	36.50	0000	0.00	0.00	0.00	000
0% 6.19 6.19 0.08 0.01 2.09 0.08 0.08 0.01 2.09 0.08 0.09 0.00 0	70.0%	3 .	4.49	3.17	11,56	0.27	1.39	90.00	0.10	1.68	0.15	10%	36.50	0.00	0.00	0.00	0.00	000
0% 8.07 7.13 4.30 12.26 0.05 0.14 3.56 0.27 10% 36.50 0.00	60.0%	6.49	5.57	3,67	11.90	934	1,51	9000	0.11	2,09	0.48	10%	36.50	00.0	0.00	0.00	0.00	000
0% 5.88 8.98 5.03 12.63 0.40 1.79 0.006 0.14 3.36 0.27 10% 36.50 0.00 0.10 0.00 0.01 0.68 12.38 12.38 13.02 0.44 1381 0.006 0.16 4.17 0.22 10% 36.50 0.00 0.10 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.02 <t< td=""><td>50.0%</td><td>8.07</td><td>7.43</td><td>4,30</td><td>12.25</td><td>0.35</td><td>1.64</td><td>900'0</td><td>0.13</td><td>797</td><td>0.22</td><td>10%</td><td>36.50</td><td>00'0</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.00</td></t<>	50.0%	8.07	7.43	4,30	12.25	0.35	1.64	900'0	0.13	797	0.22	10%	36.50	00'0	0.00	0.00	0.00	0.00
0% 12.38 11.13 5.78 13.02 0.44 1.97 0.006 0.16 4.17 0.32 10% 36.50 0.00 0.10 0.00 0.01 0% 16.07 14.23 6.81 13.55 0.50 2.08 0.006 0.21 7.18 0.50 10% 36.50 0.00 0.40 0.00 0.01 0.00 0.01 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.01 0.02 0.01 0.01 0.02	40.0%	88.6	8.98	5.03	12.63	0.40	4.2	9000	0.14	85. 85.	0.27	10%	36,50	00.0	0.40	0.00	6.04	6.0 1
0% 16.67 14.23 6.81 13.55 0.50 2.06 0.78 10.78 36.50 0.00 0.40 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00	30.0%	12.38	11.13	5.78	13,02	9.4	95	900'0	0,15	4.17	0.22	10%	36,50	0.00	0,10	0,00	0.01	0.01
0% 22.26 19.17 8.32 14.24 0.68 2.30 0.00 10.26 0.00 10.02 0.69 0.20 10.02 0.69 0.26 10.02 0.67 5% 18.25 0.90 0.40 0.02 0.00 0% 34.22 33.08 11.34 16.40 0.78 2.77 0.006 0.28 12.39 0.80 17.8 3.65 1.70 0.40 0.02 0.01 0% 40.48 37.70 13.03 16.32 2.89 0.006 0.30 14.1 0.90 1% 3.65 2.20 0.00 0.01 0.00 0.00 1% 3.65 2.29 0.00 0.01 1% 3.65 2.20 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.01 0.02 1.7 1.83 2.80 2.80 0.01 0.01 0	20,0%	16.07	14.23	8	13.55	0.50	2.08	9000	6.13	5,33	82,0	10%	36.50	000	0,10	0.00	0.01	0.04
0% 34,22 26,75 10,38 14,34 0.69 2.57 0.00 0.28 10,39 1% 5% 18,25 0.90 0.40 0.65 0.02 0.00 0.28 12,39 0.80 1% 3.65 1.70 0.65 0.02 0.01 0.01 0.02 1.23 0.80 1% 3.65 1.70 0.65 0.01 0.01 0.02 1.41 0.90 1% 3.65 1.70 0.65 0.01 0.01 0.02 0.01 0.01 0.02 1.41 0.90 1% 3.65 2.20 0.90 0.01 0.02 0.01 0.01 0.02 1.41 0.02 1.02 0.01 0.01 0.02 0.02 0.01 0.01 0.02 1.02 1.02 0.01 0.02 0.02 0.01 0.01 0.02 1.02 1.02 0.01 0.02 0.02 0.01 0.02 0.02 0.01 0.02 0.02 0.02 0.01 0.02 </td <td>10.0%</td> <td>22.26</td> <td>19,17</td> <td>8,32</td> <td>14.24</td> <td>0,58</td> <td>2,30</td> <td>9000</td> <td>0.21</td> <td>7.18</td> <td>0.50</td> <td>40%</td> <td>36.50</td> <td>8,</td> <td>0.20</td> <td>40:0</td> <td>0,02</td> <td>90'0</td>	10.0%	22.26	19,17	8,32	14.24	0,58	2,30	9000	0.21	7.18	0.50	40%	36.50	8,	0.20	40:0	0,02	90'0
0% 40.48 37.70 13.03 16.72 0.83 2.89 0.006 0.30 14.11 0.90 1% 3.65 2.20 0.90 0.02 0.01 0.01 0.% 55.23 46.36 14.38 16.32 0.92 3.09 0.01 0.33 17.36 1.06 1% 3.65 2.20 0.90 0.02 0.01 0.02 0.01 0.02 0.01 0.03 17.36 1.06 1.06 0.31 17.36 1.06 1.06 0.03 1.00 0.02 0.01 0.01 0.01 0.01 0.01 0.01	20%	34.23	26.75	10.38	14.94	0.69	2.57	0.006	0.25	10.02	0.67	26	18.25	06'0	0,40	0.05	0.02	20.0
0% 40.48 37.70 13.03 15.72 0.83 2.89 0.006 0.30 14.11 0.30 1% 3.65 2.20 0.90 0.00 0.01 0.33 17.36 1.06 1% 3.65 3.50 1.60 0.04 0.02 5% 62.74 57.49 19.31 22.46 0.86 2.98 0.006 0.31 24.52 0.96 1.83 2.80 1.60 0.01 0.01 6% 72.46 0.86 2.98 0.006 0.31 24.52 0.96 1.83 2.80 1.60 0.01 0.01 0% 78.46 0.06 0.31 24.52 0.96 1.43 2.80 0.02 0.01 0% 78.46 0.86 2.38 0.06 0.34 26.56 1.43 1.83 3.90 2.80 0.01 1 78.46 1.83 2.36 2.40 2.40 2.60 47.55 2.60 2.80 2.20	4.0%	34.92	33.08	1	15.40	0.78	2.77	900'0	0.28	12,39	0.30	1%	3.65	£.78	9.6	0.02	0.01	0.03
0% 52.23 46.36 14.98 16.32 0.92 3.09 0.01 0.33 17.36 1.06 1% 3.65 3.50 1.60 0.04 0.02 6% 62.74 57.49 19.31 22.46 0.86 2.86 6.006 0.31 21.52 0.96 1.83 26.56 1.83 2.80 1.60 0.01 0% 78.45 78.46 0.95 3.48 0.01 0.34 26.56 1.43 1.83 2.80 6.00 0.01 0% 78.46 1.83 1.83 3.90 2.80 0.00 0.01 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.01 0.01 0.02 0.02 0.01 0.02 0.02 0.01 0.02 0.01 0.02 0	3,0%	40.48	37.70	සය	15.72	0.83	2.89	9000	0.30	14,11	06.0	*	3,65	2.20	0.90	0.02	0.01	0.03
6% 62.74 57.49 19.31 22.46 0.86 2.98 0.006 0.31 21.52 0.96 1% 1.83 2.60 1.60 0.01 0.01 0.01 0.01 0.01 0.01 0	2.0%	52.23	46.36	14.99	16.32	0.92	3.09	0.01	0.33	17.36	4.06		3,65	3,50	1,60	0.04	0.02	0.06
0% 79.16 70.95 23.41 0.05 3.18 0.01 26.56 1.13 1% 1.83 3.90 2.80 0.02 0.01 Total annual sediment yield (bertload and supported	15%	62.74	57.49	19.34	22.46	0.86	2.98	6.006	0.34	24.52	96.0	1%	1.83	2.60	1,60	0.01	0.01	0,02
Total annual sediment yield (betthad and superoded 73.0 47.5 sand bed-material load) (tons/yt): Upstream total annual sediment supply 76.0 51.0 bifference in sediment transport capacity (tons/yt) (Worksheet 5-12a) (supply 76.0 51.0 bifference in sediment transport capacity (tons/yt) (+ cr -): Stability evaluation: Degradation or Stability evaluation: Degradation or Stability	40%	79.45	70.95	22.29	23.41	0.95	3.48	0.01	0.34	36.56	1.13	*	1.83	3.30	2.80	0.02	0.01	0.03
total arrural sediments upply 76.0 51.0 (tors/x) (Worksheet 5-12a) 76.0 51.0 13 ediment transport capacity 3.0 3.0 3.6 (tors/x) (+ cr -): (tors/x) (+ cr -): Stable:	Nde:	U	-00								Total enm	sal sedimer	it yield (bec and bed-mo	load ands ite ial load)	(tons/y):	73.0	47.5	120.5
Aggradation, Degradation or Stable:												Upstre	am total an (tors/yr)	Nual sedimi (Workshe	entsupply et 5-12a):	76.0	51.0	127.0
												Diffeenc	a in sedima	ant trenspoa (tons (yri)	tospacity (+ or - };	3.0	3.6	9'9
												ty evaluatic		ation, Degr.	Stable:			

Copyright @ 2005 Wildland Hydrology



RB

Worksheet 5-10. Summary form of annual streambank erosion estimates for various study reaches.

Stream: N	lacgruder Day	/ 3, Reach - R	each 1	Location	:		·····	
Graph Used:		Total Bai	nk Length (ft):	242		Date:	9/26/2007	
Observers:			Valley Type:			Stream Type:		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
Station (ft)	BEHI rating (Worksheet 5-8) (adjective)	NBS rating (Worksheet 5-9) (adjective)	Bank erosion rate (Figure 5-38 or 5- 39) (ft/yr)	Length of bank (ft)	Study bank		Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}	
1. RB 201-209	Moderate	Low	0.1084821	8	2.8	2.43	0.01	
2. RB 225-240	Low	Moderate	0.09	15	1.6	2.16	0.01	
Station 006 - 3. 02 5 R	Low	Extreme	1.9986418	19	3.1	117.72	0.30	
Station 025 - 4. 029 R Station 029 -	Moderate	Extreme	2.0039063	4	3.2	25.65k#	0.31	
5. 039 R Station 045-	High	Low	1.9996875	10	3.2	63.99	0.31	
6. 048 rb Station 048-	High	Low	0.1928571	3	2.8	1,62	0.03	ē
7. 063 rb Station 063-	High	Very Low	0.2290909	15	2.2	7.56	0.02	
8. 072rb Station 099-	High	Low	0.4	99	3.3	11.88	0.06	9
9. 111rb Station 111-	Moderate	Low	0.0964286	12	2.1	2.43	0.01	ē
10. 122 rb	Moderate	Low	0.0954545	11	1.8	1.89	0.01	
14.					gramman (sec) 2 E) V
1 2.	Kili is Williams							Ģ
13.		elines da culta a precore por se Estados					TE IVETI	
14.	Su Sille di Chiana da deservici			en roj governo sporo a	epop pagenta and the con-			RB
IS			(ax 727)		Total	4 1 X		To
Sum erosion su	btotals in Colu	mn (7) for eac	h BEHI/NBS (combination	erosion (ft³/yr) Total	237.33		3
Convert erosion	in ft ³ /yr to yds	³ /yr {divide To	otal erosion (ft	³ /yr) by 27}	erosion (yds³/yr)	8,79		
Convert erosion by 1.3}	in yds ³ /yr to to	ons/yr (multipl	y Total erosio	n (yds³/yr)	Total erosion (tons/yr)	11.43		
Calculate erosic (tons/yr) by total				erosion	Total erosion (tons/yr/ft)	0.0472		,0

Worksheet 5-10. Summary form of annual streambank erosion estimates for various study reaches.

Stream: N	lacgruder Day	/ 3, Reach - L	EFT BANK B	I Location	:		
Graph Used:		Total Ba	nk Length (ft):	242		Date	12/30/1999
Observers:			Valley Type:			Stream Type	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	T (8)
Station (ft)	BEHI rating (Worksheet 5-8) (adjective)	NBS rating (Worksheet 5-9) (adjective)	Bank erosion rate (Figure 5-38 or 5- 39) (ft/yr)	Length of bank (ft)	Study bank height (ft)		Erosion Rate (tons/yr/ft) {[(7)/27] × 1.3 / (5)}
GLIDE X- 1 SECT. 229		Low	0 0	HASE SECTION .	1.6	0	0.00
2. LB 220	Low	Moderate	0.10125	8	3	2.43	0.01
3. LB 66-41	Moderate	Low	0.108	25	1.6	4.32	0.01
4. LB 80-66	High	Very Low	0.2268908	14	1.7	5.4	0.02
5. LB146-132	High	Very Low	0.2285714	14	2.7	8.64	0.03
6. LB157-146	Moderate	Low	0.1	11	2.7	2.97	0.01
7. LB168-157	High	Low	0.2045455	14	1.2	2.7	0.01
8. LB195-206	Moderate	Low	0.1125	16	2.7	4.86	0.01
9. LB204-214	High	Extreme	1.4989967	23	2.6	89.64	0.19
0. Pool XS032 RIFFLE X-	Extreme	Extreme	3.96	1	3	11.88	0.57
1. SEC 136,25	High	Very Low	0.216	To real experiences in	2.5	0.54	0.03
2.			12 -41-475				
3			lidaji wax	(W, ma, <u>uu-</u>			
4.							
5. Sum erosion su	btotals in Colu	mn (7) for eac	h BEHI/NBS d	combination	Total erosion		
Convert erosion	in ft³/yr to yds	³ /yr {divide To	otal erosion (ft	³ /yr) by 27}	(ft ³ /yr) Total erosion (yds ³ /yr)	133.38	
Convert erosion by 1.3}	in yds ³ /yr to to	ons/yr (multip!	y Total erosio	n (yds³/yr)	Total erosion (tons/yr)	6.42	
Calculate erosio (tons/yr) by total				erosion	Total erosion (tons/yr/ft)	0.0265	

3rd Field Day

a. Riparian Vegetation

Worksheet C-4. Riparian vegetation composition/density used for channel stability assessment.

	SSITIETAL.		Dinasias Va	AND THE PROPERTY OF THE	Samuel Color
	41		Riparian Ve	egetation	
Stre	Magner Dam:			Location: Reach	/
Obs	servers: Teen	1	Reference reach	Disturbed (impacted reach) Date:	9 25/07
Exis spe con	cies Julip Per position: Mixeu	ler Donnina Riporten Ho	reduced	Potential BAK-HALA species composition: MIKE HAM	
	iparian cover categories	Percent aerial cover*	Percent of site coverage**	Species composition	Percent of total species composition
1. Overstory	Canopy layer	95	10	Tuliptopbe MAPLE Maple Sycamore Association	#0 75 20 % 25 2.5
					100%
2. Understory	Shrub layer		25	elultitlerakeise Spice Bush Aluete Var berry Issan Wood Service borry	10 b0 5 20
					100%
levei	Herbaceous		40 35	Tapsnese Hiltyass Clear Weed Plantain Crolden Rod Honey snell Roar Feen	60 5 5 5
3. Ground level	Leaf or needle litter		20	Remarks: Condition, vigor and/or usage of existing reach:	100%
	Bare ground		10		
	d on crown closure. ed on basal area to	surface area.	Column total = 100%		

3rd Field Day

b. Flow Regime

Worksheet C-5. Flow Regime variables that influence channel characteristics, sediment regime and biological interpretations.

			FLOW	REGIN	ΛE				
Stream:	<u></u>		Location	n:			1		
Observers:							Date:		
	COMBINATIONS that	P2	P8						
General (Category							, III	3
Έ,	Ephemeral stream cha with intermittent.								
S	Subterranean stream surface flow that follow			allel to an	nd near the	surface f	or various	seasons	s - a sub-
· •	Intermittent stream ch involve springs, snowr reappear along variou	nelt, artifi	icial contr	ols, etc. (Often this to	erm is as			
Р	Perennial stream char	nels: su	rface wat	er persist	s yearlong.				
Specific (Category					ال الله عرب			
1	Seasonal variation in s	treamflo	w domina	ted prima	rily by sno	vmelt run	off.		-
2.	Seasonal variation in s	treamflo	w domina	ted prima	rily by stori	mflow run	off.		
3	Uniform stage and ass	ociated s	streamflov	v due to s	pring-fed o	ondition,	backwate	er, etc.	
4	Streamflow regulated	by glacial	melt.		ш.				
5	Ice flows/ice torrents for	om ice d	am breac	hes.			44.1		
6	Alternating flow/backw	ater due	to tidal in	fluence.		-			
7	Regulated streamflow	due to di	versions,	dam rele	ase, dewat	ering, etc			
8	Altered due to develop conversions (forested								
9	Rain-on-snow generate	ed runoff							

3rd Field Day

c. Stream Size and Order

Worksheet C-6. Stream size/order categories for stratification by stream type.

	Stream Siz	e and Order	
Stream:			
Location:			
Observers:			
Date: Stream Size	e Category and	l Order 🤝	54(2)
Category	STREAM SIZ	dth	Check (🗸) appropriate
	meters	feet 🦠	category
S-1	0.305	<1	
S-2	0.3 – 1.5	1 – 5	
S-3	1.5 - 4.6	5 - 15	
S-4	4.6 - 9	15 – 30	P
S-5	9 – 15	30 – 50	13
S-6	15 – 22.8	50 – 75	
S-7	22.8 - 30.5	75 – 100	
S-8	30.5 – 46	100 – 150	
S-9	46 – 76	150 – 250	
S-10	76 – 107	250 – 350	
S-11	107 – 150	350 – 500	П
S-12	150 – 305	500 – 1000	
S-13	>305	>1000	. []
	Stream	n Order	

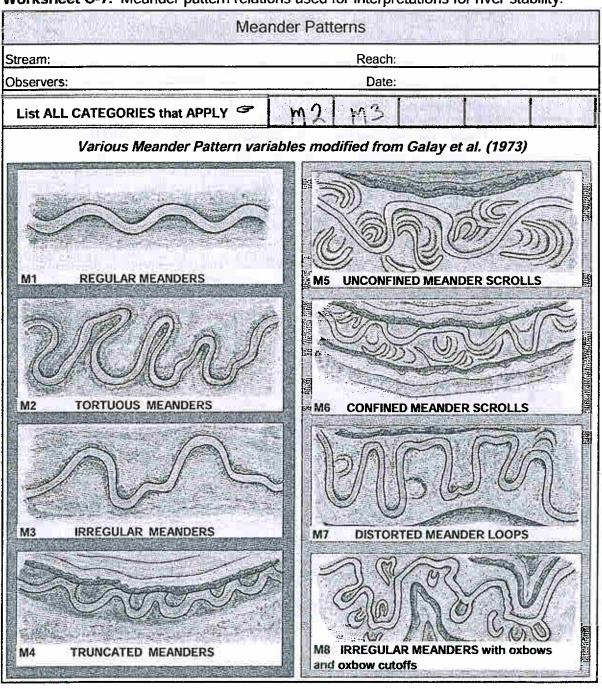
reach. For example a third order stream with a bankfull width of 6.1 meters (20 feet) would be indexed as: S-4(3).

Add categories in parenthesis for specific stream order of

3rd Field Day

d. Meander Patterns

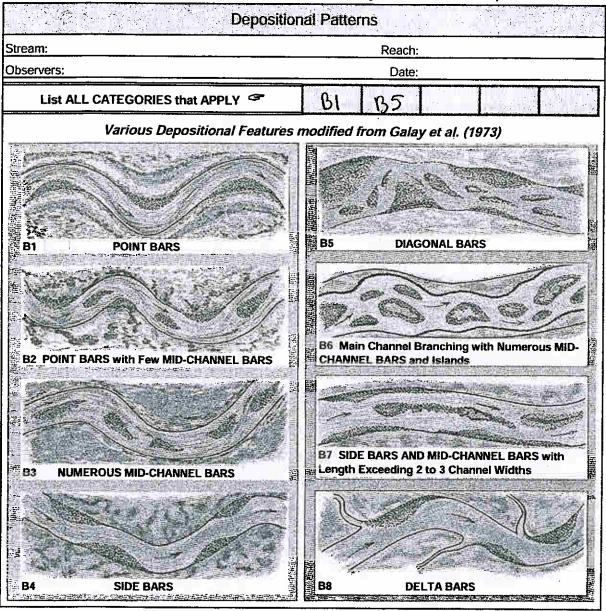
Worksheet C-7. Meander pattern relations used for interpretations for river stability.



3rd Field Day

e. Depositional Patterns

Worksheet C-8. Depositional patterns used for stability assessment interpretations.



3rd Field Day

f. Channel Blockages

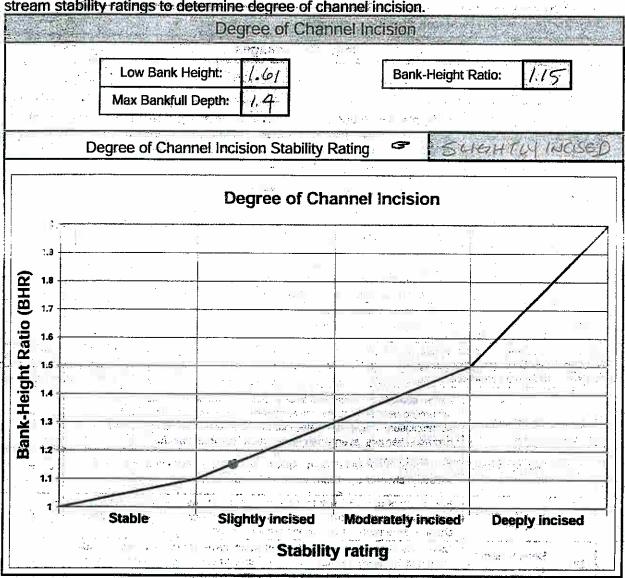
Worksheet C-9. Various categories of in-channel debris, dams and/or channel blockages used to evaluate channel stability.

	英国新疆	Channel Blockages,	
Strea	m:	Location:	The same of the sa
Obse	rvers:	Date:	
Desc	ription/extent	Materials, which upon placement into the active channel or flood- prone area, may cause adjustments in channel dimensions or conditions due to influences on the existing flow regime.	Check (//) all that apply
D1	None	Minor amounts of small, floatable material.	E
) 2	nfrequent	Debris consists of small, easily moved, floatable material, e.g., leaves, needles, small limbs and twigs.	С
D3	Moderate	Increasing frequency of small- to medium-sized material, such as large limbs, branches and small logs, that when accumulated, affect 10% or less of the active channel cross-section area.	~
D4	Numerous	Significant build-up of medium- to large-sized materials, e.g., large limbs, branches, small logs or portions of trees that may occupy 10–30% of the active channel cross-section area.	k j
D5	Extensive	Debris "dams" of predominantly larger materials, e.g., branches, logs and trees, occupying 30–50% of the active channel cross-section area, often extending across the width of the active channel.	Ē
D6	Dominating	Large, somewhat continuous debris "dams," extensive in nature and occupying over 50% of the active channel cross-section area. Such accumulations may divert water into the flood-prone areas and form fish migration barriers, even when flows are at less than bankfull.	
D 7	Beaver dams: Few	An infrequent number of dams spaced such that normal streamflow and expected channel conditions exist in the reaches between dams.	
D8.	Beaver dams: Frequent	Frequency of dams is such that backwater conditions exist for channel reaches between structures where streamflow velocities are reduced and channel dimensions or conditions are influenced.	G
D9	Beaver dams: Abandoned	Numerous abandoned dams, many of which have filled with sediment and/or breached, initiating a series of channel adjustments, such as bank erosion, lateral migration, avuision, aggradation and degradation.	
D10	Human influences	Structures, facilities or materials related to land uses or development located within the flood-prone area, such as diversions or low-head dams, controlled by-pass channels, velocity control structures and various transportation encroachments that have an influence on the existing flow regime, such that significant channel adjustments occur.	□

3rd Field Day

g. Degree of Channel Incision (Bank-Height Ratio)

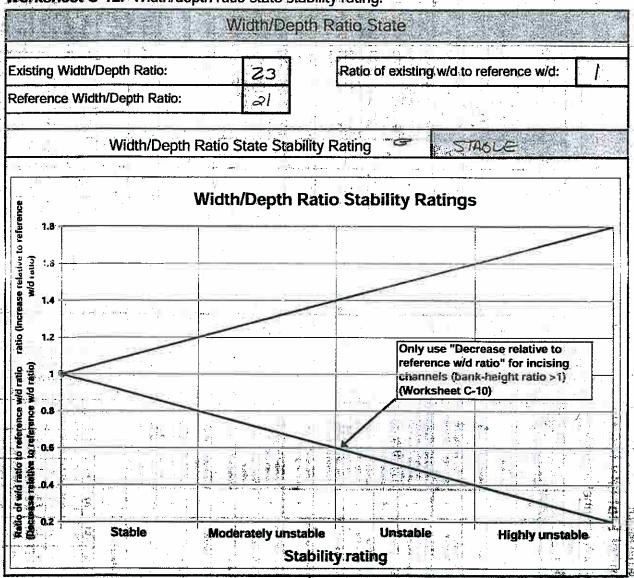
Worksheet C-10. Relationship of Bank-Height Ratio (BHR) ranges to corresponding stream stability ratings to determine degree of channel incision.



3rd Field Day

i. Width/Depth Ratio State

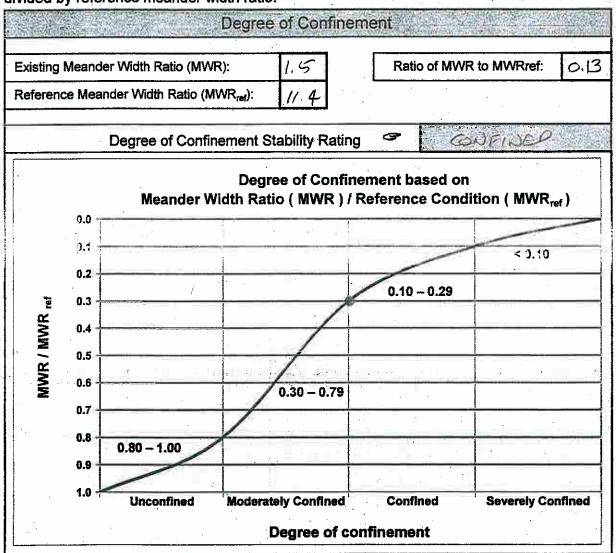
Worksheet C-12. Width/depth ratio state stability rating.



3rd Field Day

j. Degree of Channel Confinement (Meander Width Ratio (MWR))

Worksheet C-13. Degree of confinement stability ratings based on meander width ratio divided by reference meander width ratio.



3rd Field Day

Worksheet C-19. Stability ratings for corresponding successional stage shifts of stream types. Check (✓) the appropriate stability rating.

Stream:	Stream Type:
Location:	Valley Type:
Observers:	Date:
Stream type changes due to successional stage shifts (Figure C-5)	Stability rating (check appropriate rating)
Stream type at potential, $(C \rightarrow E)$, $(F_b \rightarrow B)$, $(G \rightarrow B)$, $(F \rightarrow B_c)$, $(F \rightarrow C)$, $(D \rightarrow C)$	Stable
c-wider c	Moderately unstable
(G→F), (F→D), (C→F)	Unstable
(C→D), (B→G), (D→G), (C→G), (E→G)	Highly unstable

3rd Field Day

Worksheet C-20. Lateral stability prediction summary.

Stream:			Stream T	уре:	
Location:			Valley T	уре:	
Observers:			D	ate:	
Lateral stability criteria		Lateral stabili	ty categories		Selected
(choose one stability category for each criterion 1–5)	Stable	Moderately unstable	Unstable	Highly unstable	points (from each row)
W/d ratio state (Worksheet C-12)	< 1.2	1.2 – 1.4	1.4 – 1.6	> 1.6	2
	(2)	(4)	(6)	(8)	
Depositional pattern (Worksheet C-8)	B1, B2	B4, B8	. Вз	B5 B6, B7	4
<u> </u>	(1)	(2)	(3)	. (4)	
Meander pattern (Worksheet C-7)	M1 (V3)V/4		/12, M5, M6, M7, M8		7
·	(1)		(3)		1
Dominant BEHI / NBS (Worksheet C-16)	L/VL, L/L, L/M, L/H, L/VH, M/VL	ML MM, MH, L/Ex, H/L	MVH, MEx, H/L, H/M, H/H, VH/VL, Ex/VL	H/H, H/Ex, Ex/M, Ex/H, Ex/VH, VH/VH, Ex/Ex	4
. The second was a second	(2)	(4)	(6)	(8)	
Degree of confinement (MWR / MWR _{ref}) (Worksheet C-	0.8 1.0	0.3 – 0.79	0.1 – 0.29	< 0.1	3
13)	(1)	(2)	(3)	(4)	ger eine die er einer eine Lieuwitz
History of the control of the contro				Total points	X
	Lat	eral stability ca	itegory point r	inge	· · · · · ·
Overall lateral stability category (use total points and check stability rating)	Stable 7 – 9	Moderately unstable 10 – 12	Unstable 13 – 21	Highly unstable	

20.0

River Assessment and Monitoring: Impaired Reach

Worksheet C-18. Sediment competence calculation form to assess bed stability.

Stream:	Macq	ruder	Stream Type:									
Location:	J		Valley Type:									
Observers:			Date:	9/26	.107							
Enter rec	uired info	rmation										
34:29	D ₅₀	Riffle bed material D ₅₀ (mm)	e chanv	ul								
9.4	D ₅₀	Bar sample D ₅₀ (mm)										
.23	D _{max}	Largest particle from bar sample (ft)	70	(mm)	304.8 mm/ft							
,006	S	Existing bankfull water surface slope (ft/ft)										
1.2	d Existing bankfull mean depth (ft)											
γ_s Submerged specific weight of sediment												
Select the appropriate equation and calculate critical dimensionless shear stress												
2.2 $D_{50}/D_{50}^{^{^{^{^{^{^{^{^{^{^{^{^{^{^{^{^{^{^{$												
2.04	D _{max} /D ₅₀	Range: 1.3 – 3.0 7, 35 Use EQUATION 2	τ* = 0.038	34 (D _{max} /[O ₅₀) -0.887							
.02	τ*	Bankfull Dimensionless Shear Stress	EQUATIO	N USED:	Dmax							
Calculate	bankfull n	nean depth required for entrainment of	largest parti	cle in bar	sample							
1.30	ď	Required bankfull mean depth (ft)	$d = \frac{\tau * \gamma}{}$	S Dmax f+.								
	Check:	Г(Stable)	Stable, tren	d trod.	aggrading							
Calculate sample	bankfull w	rater surface slope required for entrain	ment of large	est particl	e in bar							
,006	s	Required bankfull water surface slope (ft/ft)	$S = \frac{\tau * \gamma}{2}$	SDmax ft.	=1.3							
	Check:	Stable □ Aggrading □ Degrading										
Sediment	competen	ce using dimensional shear stress										
.45	Bankfull si	near stress $\tau = \gamma dS$ (ibs/ft²) (substitute hydrau	lic radius, R, w	ith mean de	epth, d)							
80	Moveable	particle size (mm) at bankfull shear stress (Figu	ire C-4)									
,33	Predicted :	shear stress required to initiate movement of D _{rr}	ax (mm) (Figur	e C-4)								
∂,88	Predicted :	mean depth required to initiate movement of D _{mi}		τ γS								
.006	Predicted s	slope required to initiate movement of D_{max} (mm	$S = \frac{\tau}{yd}$									

3rd Field Day

Worksheet C-21. Vertical stability prediction for excess deposition/aggradation.

Stream:			Stream Type:		i.							
Location:	•.	,	Valley Type:									
Observers:			Date:									
Vertical stability	Vertical stabil	Vertical stability categories for excess deposition / aggradation										
criteria (choose one stability category for each criterion 1–6)	No deposition	Moderate deposition	Excess deposition	Aggradation	Selected points (from each row)							
Sediment 1 competence (Worksheet C-18)	Sufficient depth and/or slope to transport largest size available	Trend toward insufficient depth and/or slope- slightly incompetent	Cannot move D ₃₅ of bed material and/or D ₁₀₀ of bar material	Cannot move D ₁₆ of bed material and/or D ₁₀₀ of bar or sub- pavernent size	2							
· .	(2)	(4)	(6)	(8)								
Sediment capacity (POWERSED)	Sufficient capacity to transport annual load	Trend toward insufficient sediment capacity	Reduction up to 25% of annual sediment yield of bedload and/or suspended	Reduction over 25% of annual sediment yield for bedload and/or suspended	4							
	(2)	(4)	(6)	, (8).								
W/d ratio state (Worksheet C-12)	1.0 – 1.2	1.2 – 1.4	1.4 – 1.6	>1.6	Ż							
L=	(2)	(4)	(6)	(8)								
Stream succession 4 states (Worksheet (19)		(E→C)	(C→High w/d C), (B→High w/d B), (C→F).	(C→D), (F→D)	6							
	(2)	(4)	(6)	(8)	Bernauf Land S.							
Depositional 5 patterns (Workshee C-8)	L	B2, B4	B3, B5	B6, B7, B8	3							
3-0)	(1)	(2)	(3)	(4)								
Debris / blockages (Worksheet C-9)	D1, D2(D3)	D4, D7		*D6, D9, D10								
	, w	(2)	(3)	(4)								
	Carrier des	14. 24.	MUTANTAN TENEN	Total points	K,							
Supplied the state of the state	Vertical stabi		nt range for exces idation	s deposition /								
Vertical stability for excess deposition / aggradation (use total points and check stability rating)	No deposition ty 10 – 14 □	Moderate deposition 15 – 20	Excess deposition 21 – 30	Aggradation > 30 □	24							

3rd Field Day

Worksheet C-22. Vertical stability prediction for channel incision/degradation.

Stream:	:	ui.	Stream Type:		
Location:			Valley Type:		
Observers:			Date:		
Vertical stability	Vertical stabi				
criteria (choose one stability category for each criterion 1-5)	Not incised	Slightly incised	Moderately incised	Degradation	Selected points (from each row)
Sediment 1 competence (Worksheet C-18)	Does not indicate excess competence	Frend to move larger sizes than 'D ₁₀₀ of bar or > D ₈₄ of bed	D ₁₀₀ of bed moved	Particles much larger than D ₁₀₀ of bed moved	2
	(2)	HA (4)	(6)	(8)	
Sediment capacity (POWERSED)	Does not indicate excess capacity	Slight excess energy: up to 10% increase above reference	Excess energy sufficient to increase load up to 50% of annual load	Excess energy transporting more than 50% of annual load	2
	(2)	(4)	(6)	(8)	
Degree of channel 3 incision (BHR) (Workshet C-10)	1.00 – 1.10	1.11 – 1.30	1.31 – 1.50	> 1.50	?
(WORSHELC-10)	(2)	(4)	(6)	(8)	
Stream succession 4 states (Worksheets C-19 and C-10)	Does not indicate incision or degradation	If BHR > 1.1 and stream type has w/d between 5–10	If BHR > 1.1 and stream type has w/d less than 5	(B→G), (C→G), (E→G), (D→G)	2
	(2)	(4)	(6)	(8)	
Confinement (MWR 5 / MWR _{ref})	0.80 – 1:00	0.30 - 0.79	0.10 →0.29	< 0.10	3
(Worksheet C-13)	(1).	(2)	(3)	(4)	e. —
				Total points	12
	Vertical stab	lity category poin degrad		nel incision /	Mar.
Vertical stability for channel inclsion/ degradation (use total points and check stability rating)	Not incised 9 – 14	Slightly incised	Moderately incised 19 – 27	Degradation > 27	

3rd Field Day

Worksheet C-23. Channel enlargement prediction summary.

Stream:			Stream Type:							
Location:	75. ^{75.}		Valley Type:		n zi					
Observers:	to the state of th		Date:							
Channel enlargement	Channel enlargement prediction categories									
prediction criteria (choose one stability category for each criterion 1–4)	No increase	Slight increase	Moderate Increase	Extensive	Selected points (from each row)					
Successional stage 1 shift (Worksheet C- 19)	Stream type at potential, ($C\rightarrow E$), ($F_b\rightarrow B$), ($G\rightarrow B$), ($F\rightarrow C$), ($D\rightarrow C$)	(E→C) <i>C→</i> > <i>C</i> ~/	(G→F), (F→D)	(C→D), (B→G), (D→G), (C→G), (E→G), (C→F)	4					
	(2)	(4)	- (6)	(8)						
Lateral stability Worksneet C-20)	Stable	Moderately unstable	Unstable	Highly unstable	6					
	(2)	(4)	(6)	(8)						
Vertical stability excess deposition/ aggradation	No deposition	Moderate deposition	Excess deposition	Aggradation	40					
(Worksheet C-21)	(2)	(4)	(6)	(8)	1) 4					
Vertical stability 4 incision/ degradation (Worksheet C-22)	Not incised	Slightly incised	Moderately incised	Degradation	4					
	(2)	(4)	(6)	(8)						
	en e	And the second of the second o		Total points	X 2					
š.		Category	oint range	Accommendation	Edge Till					
Channel enlargement prediction (use total points and check stability rating)	No increase 8 – 10	Slight increase	Moderate Increase 17-24	Extensive > 24						

3rd Field Day

Worksheet C-24. Overall sediment supply rating determined from individual stability rating categories.

Stream:			Stream Type	<u> </u>					
Location:	e e e e e e e e e e e e e e e e e e e	Marke to After South	Valley Type						
Observers:	(d 1		Date						
Overall sediment supply prediction criteria (choose corresponding points for each criterion 1–5)	Stabili	ty rating	Points	Selected points					
	Stable		1	The state of the s					
Lateral stability	Mod. unsta	ble	2	10					
(Worksheet C-20)	Unstable	•	3	1 P4					
	Highly unst	able	(4)	1 ' /					
Vertical stability	No depositi	on	1						
excess deposition/	Mod. depos	ition	2	1 6					
aggradation	Excess dep	osition	3	1 43					
(Worksheet C-21)	Aggradatio	a	- 4 ¹ Bu						
Vertical stability	Not incised	· · · · · · · · · · · · · · · · · · ·	1	10					
channel incision/	Slightly inc	ised	2						
degradation	Mod. incise	d	3	6					
(Worksheet C-22)	Degradation		4						
	No increase	1	1.41						
Channel enlargement 4 prediction (Worksheet	Slight incre								
C-23)	Med, increa								
	Extensive		4						
Pfankuch channel	Good: stabl	1 :							
5 stability (Worksheet C-	Fair: mod u	nstable	2						
11)		Company 12 miles	- 10 H						
1 18/ T/7/11/11/7	Poor: unsta	ble	4						
And the second of the second o	** ** ** ** ** ** ** ** ** ** ** ** **	The same of the contract of th	Total Points	Xo					
		•		(*					
I	Category point range								
		Valegury (onic range						
Overall sediment supply rating (use total points	Low 5	Moderate 6 – 10	High 11 – 15	Very High 16 – 20					
and check stability rating)	Ľ			10 – 20					

River Assessment and Monitoring: Impaired Reach

Worksheet C-25. Summary of stability condition categories.

		T=	17.5	1
	Channel Dimension	Observers:	Stream:	
Mean	Mean bankfull depth (ft): /, 4			
	Mean bankfull (ft): ヱ゚ゔ, ゆ			960
1	3, 6 Cross	Date:		71001
	Cross-section area (ft²): 28	Stream T	Location:	
	Width of flood- prone area (ft):	m Type: <i>C牛</i>		
	(Pati	Valley Ty		
	benchment 7,3	ype: \7777		
	in.	ŋ	3 1 3	

(Channel Source)	ĮŽ	Vertical Stability (Degradation)	Vertical Stability (Aggradation)		Successional Stage Shift	Entraihment/ Competence	Sediment Capacity (POWERSED)	Bank Erosion Summary			Level III Stream Stability Indices				reatures	River Profile and Bed	Channel Pattern	Channel Dimension	Observers:	Stream:
Circle: Low Moderate Agn Very high Remarks/causes:	Circle: No increase Slight increase Moderate increase Extensive Remarks/causes:	Circle: Not incised s।।প্রাথি beised Moderately incised Degradation Remarks/causes:	Circle: No deposition Mendagate deposition Excess deposition Aggradation Remarks/causes:	stable Remarl	Potential state (typ	Largest particle from $\tau = 0.33$ $\tau = 0.02$ depth _{bit} : $t = 0.08$ Required Required slope _{bit} : $t = 0.08$ Slope		ank erosion rate: Curve used: Rei 0.037年 (tons/yr/ft) にかり	Meander Width Reference Degree of confinement NWR / MWR / M	ratio (W/D): 23 ratio (W/D _{[ref}) Q/ (W/D) / (W/D _{ref}); Stability rating: STABLE	cision It Ratio): (, ໄ ວ໌ ໄລbility rating:	Iteam size $\mathcal{A}(2)$ Meander \mathcal{M}_3 Dep pattern(s); \mathcal{M}_3 pattern	ation The Popler Oak Hickory down myked	Remarks: Condition, vigor and/or usag): 1.48 3.26 spacing: 58 Valley: 000 9	ax Riffle Pool Death ratio Riffle Pool	Lm/W _{bkf} : 4.49 Rc/W _{bkf} :	Mean bankfull Mean bankfull Cross-section Width of flood- Entrenchment Cross-section width (ft): ノ, チ width (ft): 23, 6 area (ft.): 28 prome area (ft): ratio: 7,3 。	Date: Stream Type: こ今 Valley Type: 女皿 🥫	Location:

Copyright © 2007 Wildland Hydrology

Copyright © 2007 Wildland Hydrology

Worksheet C-26. Field form for documenting scour chain results and corresponding bed-elevation changes. River Assessment and Monitoring: Impaired Reach

Scenario 2 or 3. Scenario 3 or 4. Scenario 3: Sut	Scenario #1.		le R	T	1-		<u>.</u>	Observers:	Ou call Halle
or 3. or 4. Sub	io #1.	Chain #4	Chain #2	Chain #1		in.		S:	dilic.
yr 3. Scenario 2: Enter length of chain exposed. Scenario 3: Enter r. 4. Scenario 3: Enter elevation of bed at same station @ 2nd year Subtract 1st and 2nd year elevations to calculate net change in bed.		29.0	13.0	6,05	(ft)	From cross-section	i esta lo		, (II)
er length of er elevation year elevat	Scenario #2,	9802	16116	2	Elevation (ft)	s-section	ostallaulonil		A. 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Enter length of chain exposed. Enter elevation of bed at same 2nd year elevations to calculate	,	96	AR	Burn	Largest (mm)	Particles	idia (iksta)	21	4 /
Scenario 2: Enter length of chain exposed. Scenario 3: Enter le Scenario 3: Enter elevation of bed at same station @ 2nd year. Iract 1st and 2nd year elevations to calculate net change in hed		M K	0	**	2 nd Largest (mm)	_			
o 3; Enter le 2 2nd year.	Scenario #3				Scenario # (1–5)		* 1	Stream Type	
Enter length of Junia exposed in year. Scenario 4: Enter dep					Scour depth" (ft)	Chai			LOCARON.
n exposed ther Enter depth of	Scena				Elevation ^b (ft)		100	Valley Type:	
then subsequently buried. th of material over chain.	rio #4				Net change ^c (ft)		ta (2nd Year	7;	
y buried. chain.	Connecto			4	Largest (mm)	Particles		Date	
	#5 (0)				2 nd Largest (mm)	Particles near chain			

3rd Field Day

3. Channel Change

Worksheet C-28. Summary of annual data comparisons

PVOI K	sheet C-28. Summary	THE RESIDENCE OF THE PARTY OF T	0.0000000000000000000000000000000000000	son Forn			
Stream	: MAGRUDER			Reach: 1			No. of the second
Observ	: Magruder vers: Team 1		Date - Year 1:	2007	Date -	Year 2:	
		Riffi) XS .	.	IXS:	Glid	xs:
		Year 1	Year 2	Year 1	Year 2	Year 1	Year 2
£	Width _{BKF}	, 23,6		15.1	!	21.2	
Cross-section dimensions	Mean depth _{bkf}	1.2		1.6	¥ 1 1	1.3	
ens	Width/depth ratio	19.8		9.4		26.3	· .,
dim	Cross-sectional Area _{bkf}	28.01		24.4		272	
<u>ت</u> ق	Max depth _{bkf}	1.38		3.89		1.79	i
Pebble count	D ₃₅ (mm)	15.08		19	1	10.45	: 1 1 1
	D ₅₀ (mm)	30.44		34,89		18.02	
9 0	D ₈₄ (mm)	56.04		82.5		40.32	
£	BEHI rating	Highs.4	aner li	Ex 42.2		LOW 18.4	
rosi	NBS rating	VL 1.9		Ex 1.43		10W10	
Bank Erosion	Predicted erosion (ft/yr)	/m0 @.23		no tro		MD 0.02	
	Measured erosion (ft/yr)		#DAWIIII 1				V V
		Yearn	Your			Year 1	Year 2
A STATE OF THE STA	d Pfankuch Channel y Rating	101			D ₃₅ (mm)	7.85	
	leight Ratio start:	7.35			D ₅₀ (mm)	13.77	Ш
Point B	lar slope	21.8			D ₈₄ (mm)	48.02	1 1 7 2 4
Riffle L	ength/Riffle Width	037			D ₁₀₀ (mm)	70	
² ool Le	ength/Riffle Width	1.67					
8 8	S _{rii} /S	5.54		1 9	d _{ris} /d _{bid}	1.18	
	S _{run} /S	9.97		Direction less Depth Ralles	d _{run} /d _{bkf}	1.36	
Dimensionless Slope Ratios	S _p /S	0.12		Sugar Sugar	d _p /d _{bkf}	3.26	
S S	S _g /S	0.078	· · · · ·		d _g /d _{bkf}	1.42	